

AD-A182 431

EFFECTS OF INTERLACE TILT AND SCALE FACTORS IN AN
INCOHERENT REAL-TIME EL (U) ARMY MISSILE COMMAND
REDSTONE ARSENAL AL RESEARCH DIRECTORATE

1/1

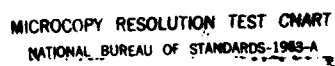
UNCLASSIFIED

AUG 86 AMSMI/TR-RD-RE-86-3 SBI-RD-E951 024 F/G 9/5

NL



END
8-87
DTIC



AD-A182 431

ADP 951 024

DTIC FILE COPY

2



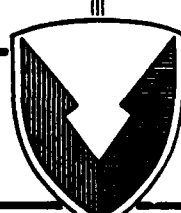
TECHNICAL REPORT RD-RE-86-3

EFFECTS OF INTERLACE, TILT AND SCALE FACTORS IN AN INCOHERENT
REAL-TIME ELECTRO-OPTICAL IMAGE CORRELATOR

John L. Johnson
Research Directorate
Research, Development, and Engineering Center

AUGUST 1986

STAMP
JUN 5 1987
A



U.S. ARMY MISSILE COMMAND

Redstone Arsenal, Alabama 35898-5000

Approved for public release; distribution is unlimited.

87 6 4 047

DISPOSITION INSTRUCTIONS

**DESTROY THIS REPORT WHEN IT IS NO LONGER NEEDED. DO NOT
RETURN IT TO THE ORIGINATOR.**

DISCLAIMER

**THE FINDINGS IN THIS REPORT ARE NOT TO BE CONSTRUED AS AN
OFFICIAL DEPARTMENT OF THE ARMY POSITION UNLESS SO DESIGNATED
BY OTHER AUTHORIZED DOCUMENTS.**

TRADE NAMES

**USE OF TRADE NAMES OR MANUFACTURERS IN THIS REPORT DOES
NOT CONSTITUTE AN OFFICIAL INDORSEMENT OR APPROVAL OF
THE USE OF SUCH COMMERCIAL HARDWARE OR SOFTWARE.**

6c. ADDRESS (City, State, and ZIP Code) Commander US Army Missile Command ATTN: AMSMI-RD-DE Redstone Arsenal, AL 35898			7b. ADDRESS (City, State, and ZIP Code)		
8a. NAME OF FUNDING/SPONSORING ORGANIZATION		8b. OFFICE SYMBOL (If applicable)		9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER	
8c. ADDRESS (City, State, and ZIP Code)			10. SOURCE OF FUNDING NUMBERS		
PROGRAM ELEMENT NO.		PROJECT NO.		TASK NO.	
				WORK UNIT ACCESSION NO.	
11. TITLE (Include Security Classification) Effects of Interlace, Tilt and Scale Factors in an Incoherent Real-Time Electro-Optical Image Correlator					
12. PERSONAL AUTHOR(S) John L. Johnson					
13a. TYPE OF REPORT Technical		13b. TIME COVERED FROM _____ TO _____		14. DATE OF REPORT (Year, Month, Day) 86 AUG	
				15. PAGE COUNT 11	
16. SUPPLEMENTARY NOTATION					
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP	Incoherent correlator Interlace scan		
			Optical correlator Integrating CCD camera		
			Real-time correlator		
19. ABSTRACT (Continue on reverse if necessary and identify by block number) The performance of an incoherent real-time optical correlator with respect to residual tilt and scale misalignment is discussed. The correlator uses CCD video data input streams and produces a real-time output in the form of a standard television video frame. The interlaced fields of the inputs and outputs are discussed and their proper use is described.					
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT. <input type="checkbox"/> DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED		
22a. NAME OF RESPONSIBLE INDIVIDUAL John L. Johnson			22b. TELEPHONE (Include Area Code)		22c. OFFICE SYMBOL AMSMI-RD-DE

TABLE OF CONTENTS

	<u>Page</u>
I. INTRODUCTION	1
II. INTERLACE EFFECTS	1
III. TILT AND SCALE EFFECTS	4
REFERENCES	5



[Handwritten checkmark]

DISTRICT OF COLUMBIA

JAN - 1968

A-1

I. INTRODUCTION

The purpose of this report is to assess the effects of several factors on the performance of the incoherent electro-optical real time correlator system. This system is based on the design proposed in references one and two by D. Psaltis. It uses an acousto-optic bragg cell to modulate a real-time video input image with a reference image which is produced by a special parallel readout high speed memory and a custom LED diode array. The correlation is read out with a CCD video camera which has been modified to perform one of the two required convolution integrals.

The factors discussed here are:

1. The interlaced input video data stream.
2. Tilt misalignments of the anamorphic optical system and residual scale differences and lateral displacement errors.

The principal elements of the system are indicated in Figure 1. The optical system O_1 transforms the M-element linear LED array into a M-line image in the AO cell. The optical system O_2 transforms the area A_1 into a rescaled area A_2 on the output CCD 2. The width D_1 corresponds to the length of the input video line from CCD 1 just as it begins to travel across the AO cell window. The detailed operation of this system is described in references 1 and 2.

II. INTERLACE EFFECTS

Consider the the output of CCD #2. It consists of N lines and is one full frame of video. It is sent to an output video monitor which writes the first N/2 lines as field #1 and the second N/2 lines as field #2. Suppose the CCD #2 is a single correlation peak. Then the monitor fields are:

Field #1: The first N/2 lines stretched 2X vertically.

Field #2. The second N/2 lines stretched 2X vertically.

The interlaced result will be the original image cut in two, the halves stretched and overlaid on each other. This is sketched in Figure 2.

In order to avoid this, we need instead, to have a field #1/field #2 flattened dual correlation peak image out of CCD #2. This is sketched in Figure 3. How can this be obtained? What we know is that the system of Figure 1 will produce correlation peaks everywhere the AO video input matches the reference image. Thus, if the video from CCD #1 is a standard field #1/field #2 sequence, then a single target scene presented to CCD #1 is converted automatically to a doubled and flattened dual target "image" as it is received by the AO cell. This is exactly the input image desired. However, the decomposition by CCD #1 of the input scene into two fields destroys half the vertical resolution. The only way to avoid this is to use a completely uninterlaced system, which is expensive and difficult in practice.

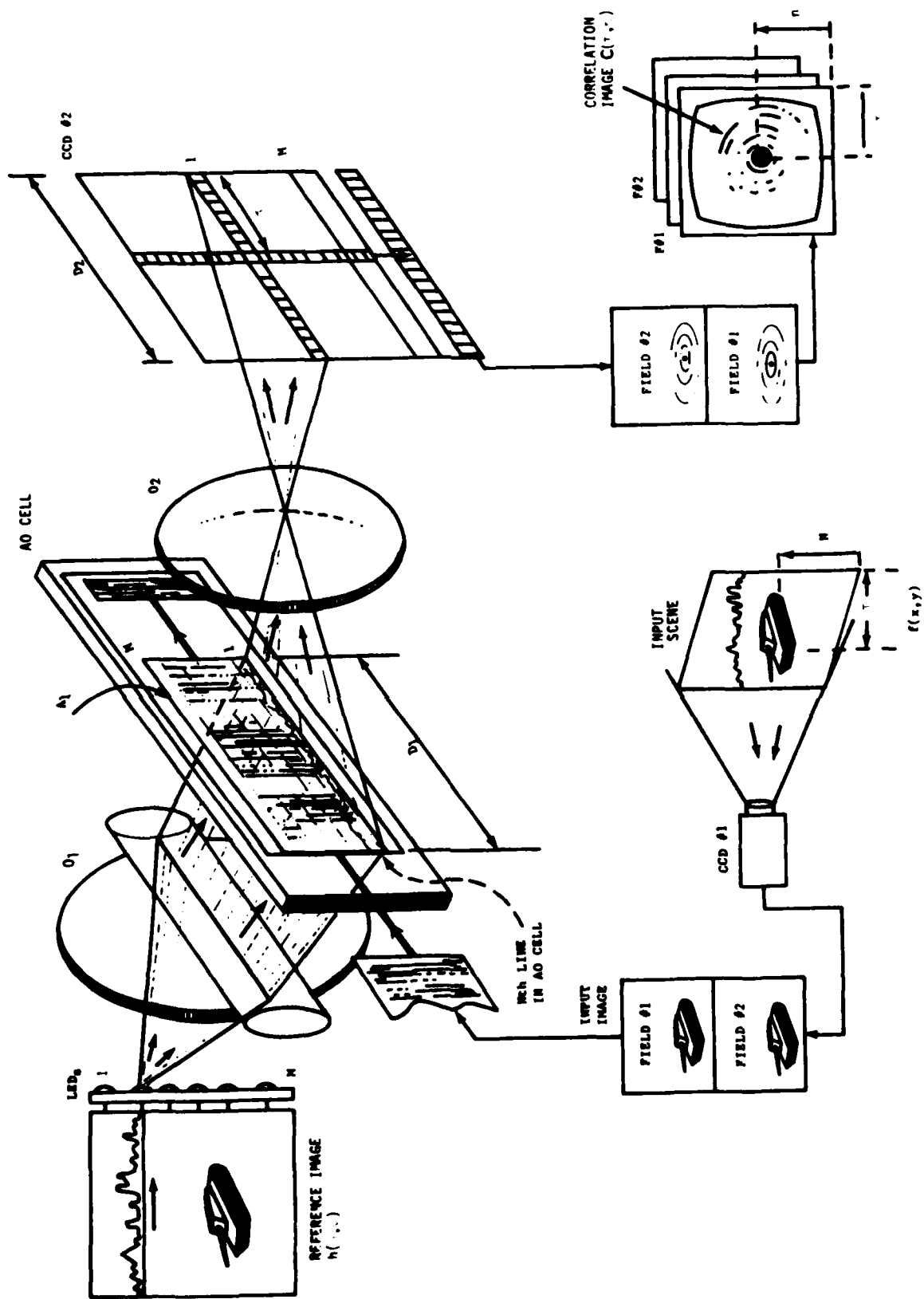


Figure 1. Correlator functions.

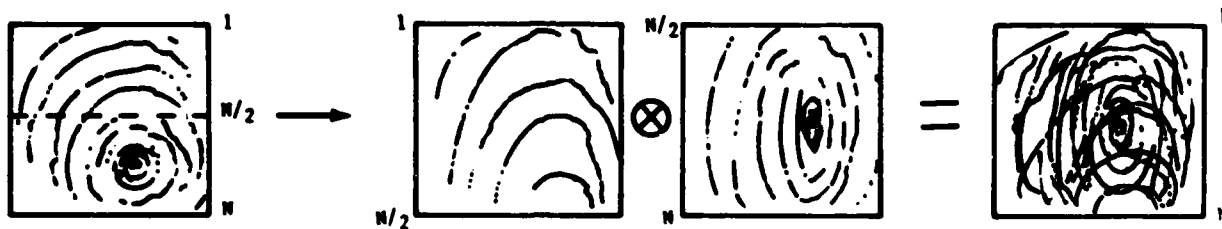


Figure 2. Uninterlaced input is scrambled by interlaced output.
Reference image has full resolution.

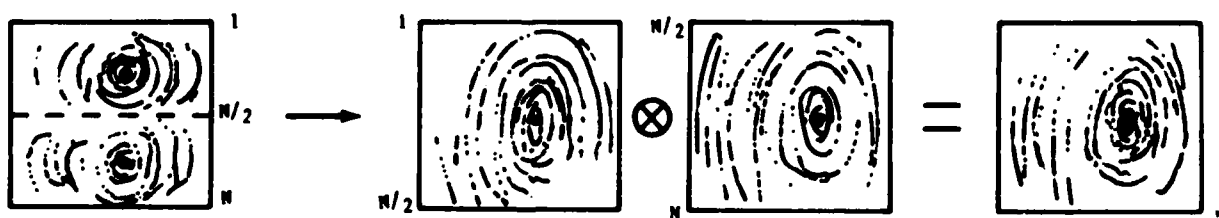


Figure 3. Good output with fully interlaced system. Reference
image has half the vertical resolution.

Thus, the use of interlace mode is appropriate for the correlator if the reference image is one field rather than one frame. The slight difference between two fields will produce an equally slight decorrelation in one field of the output; however, the other field will always be exact and thus the system should still operate satisfactorily.

III. TILT AND SCALE EFFECTS

The effects of tilt and scale changes can all be accounted for as equivalent operations on the reference image. As long as the amount of change is within the established limits of standard image correlators, usually several percent of variation, these factors will not preclude normal operation of the real-time correlator. The correlator is invariant under lateral translation of the images, so this factor should have no effect.

Mathematically, the correlation image is

$$C(\tau, n) \propto \sum_{k=n-m+1}^n \int_{T_1}^{T_1 + T_2} f(t-\tau, k) h(t, m+k-n) dt$$

and tilt and scales changes are equivalent to the transformation

$$h(u, v) \rightarrow h(u', v')$$

where

$$u' = \alpha (u \cos \theta + v \sin \theta)$$

$$v' = \beta (v \cos \theta - u \sin \theta)$$

are scaled and rotated coordinates. The scale factors (α , β) thus should be within a few percent of unity and the angular rotation θ within approximately $\pm 50^\circ$.

REFERENCES

1. Psaltis, D., Opt. Eng Vol 23, No. 1, Jan/Feb 1984, p. 12.
2. Psaltis, D., Proc. IEEE, Vol 72, No. 7, July 1984, p. 962.

DISTRIBUTION

	<u>No. Copies</u>
Commander US Army Research Office ATTN: AMXRO-PH, Dr. R. Lontz P. O. Box 12211 Research Triangle Park, NC 27709	5
US Army Research and Standardization Group (Europe) ATTN: AMXSN-E-RX, LTC D. R. Reinhard Box 65 FPO New York 09510	1
Commander US Army Materiel Development and Readiness Command ATTN: Dr. James Bender Dr. Gordon Bushey 5001 Eisenhower Avenue Alexandria, VA 22333	1 1
HQDA Office of DCS for RD&A ATTN: DAMA-ARZ Room 3A474, The Pentagon Washington, DC 20301	1
OUSDR&E Room 3D1079, The Pentagon Washington, DC 20301	1
Director Defense Advanced Research Projects Agency (STO) ATTN: CDR T. F. Weiner D. W. Waish 1400 Wilson Boulevard Arlington, VA 22209	1 1
OUSDR&E ATTN: Dr. G. Gamota Dep. Asst. for Research (Adv. Technology) Room 3D1067, The Pentagon Washington, DC 20301	1
Director of Defense Research and Engineering Engineering Technology Washington, DC 20301	1
Commander US Army Aviation Systems Command 12th and Spruce Streets St. Louis, MO 63166	1

Director US Army Air Mobility R&D Laboratory Ames Research Center Moffett Field, CA 94035	1
Commander US Army Electronics R&D Command ATTN: AMSEL-TL-T, Dr. Jacobs DELEW-R, Henry E. Sonntag Fort Monmouth, NJ 07703	1 1
Director US Army Night Vision Laboratory ATTN: John Johnson John Deline Peter VanAtta Fort Belvoir, VA 22060	1 1 1
Commander US Army Picatinny Arsenal Dover, NJ 07801	1
Commander US Army Harry Diamond Laboratories 2800 Powder Mill Road Adelphi, MD 20783	1
Commander US Army Foreign Science and Technology Center ATTN: W. S. Alcott 220 7th Street, NE Charlottesville, VA 22901	1
Commander US Army Training and Doctrine Command Fort Monroe, VA 22351	1
Commander US Naval Air Systems Command Missile Guidance and Control Branch Washington, DC 20301	1
Chief of Naval Research Department of the Navy Washington, DC 20301	1
Commander US Naval Air Development Center Warminster, PA 18974	1
Commander, US Naval Ocean Systems Center Code 6003, Dr. Harper Whitehouse San Diego, CA 92152	1

Director, Naval Research Laboratory	
ATTN: Dave Ringwolt	1
T. Gialborinzi, Code 5570	1
Washington, DC 20390	
 Commander, Rome Air Development Center	
ATTN: James Wasielewski, IRRC	1
Griffiss AFB, NY 13440	
 Commander, US AFORSR/NE	
ATTN: Dr. J. A. Neff	1
Bolling AFB, Bldg 410	
Washington, DC 20332	
 Commander	
US Air Force Avionics Laboratory	
ATTN: D. Rees	1
W. Schoonover	1
Dr. E. Champaign	1
Dr. J. Ryles	1
Gale Urban	1
David L. Flannery	1
Wright Patterson AFB, OH 45433	
 Environmental Research Institute of Michigan	
Radar and Optics Division	
ATTN: Dr. A. Kozma	1
Dr. C. C. Aleksoff	1
Juris Upatnieks	1
P. O. Box 8618	
Ann Arbor, MI 41807	
 ITT Research Institute	
ATTN: GACIAC	1
10 W. 35th Street	
Chicago, IL 60616	
 Dr. J. G. Castle	
9801 San Gabriel, NE	1
Albuquerque, NM 87111	
 Dr. J. W. Goodman	
Information Systems Laboratory	
Department of Electrical Engineering	1
Stanford University, CA 04305	
 Eric G. Johnson, Jr.	
National Bureau of Standards	1
325 S. Broadway	
Boulder, CO 80802	

Dr. Nicholas George The Institute of Optics University of Rochester Rochester, NY 14627	1
Naval Avionics Facility Indianapolis, IN 46218	1
Dr. David Cassasent Carnegie Mellon University Hamerschage Hall, Room 106 Pittsburg, PA 15213	1
Professor Anil K. Jain Department of Electrical Engineering University of California, Davis Davis, CA 95616	1
Terry Turpin Department of Defense 9800 Savage Road Fort George G. Meade, MD 20755	1
Dr. Stuart A. Collins Electrical Engineering Department Ohio State University 1320 Kennear Road Columbus, OH 43212	1
US Army Materiel Systems Analysis Activity ATTN: AMXSY-MP Aberdeen Proving Ground, MD 21005	1
US Army Night Vision Laboratory ATTN: DELNV-L, Dr. R. Buser Ft. Belvoir, VA 22060	1
Dr. F. T. S. Yu Penn State University Department of Electrical Engineering University Park, PA 16802	1
Dr. William P. Bleha Liquid Crystal Light Valve Devices Hughes Aircraft Company 6155 El Camino Carlsbad, CA 92008	1

AMSMI-RD, Dr. McCorkle	1
Dr. Rhoades	1
-RD-DP, Jerry Hagood	1
-RD-AC	1
-RD-AS, W. Pittman	1
-RD-GC, J. A. Mclean	1
-RD-RE, Dr. R. L. Hartman	1
Dr. J. S. Bennett	1
Dr. C. M. Bowden	1
Dr. J. L. Johnson	80
-RD-SS	1
-RD-CS-R	15
-RD-CS-T, Record Copy	1
-GC-IP, Mr. Bush	1
AMCPM-PE-E, John Pettitt	1
-PE	1

END

8-87

DTIC